

### HB 219 Worked Example 3.6.1 Extensive Urban MEN System Supplied by a HV Overhead Line

2 km aerial HV feed to a pole-mounted distribution transformer, no OHEW, common HV/LV earth extensive MEN, LV neutral not bonded to HV source substation.

**11 kV source, no NER.**

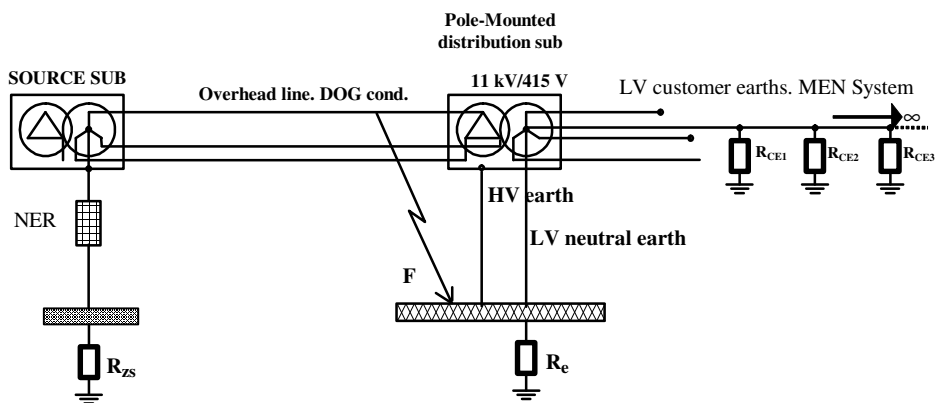


Fig. 3.6.1.1 Extensive urban MEN network supplied by a HV overhead line

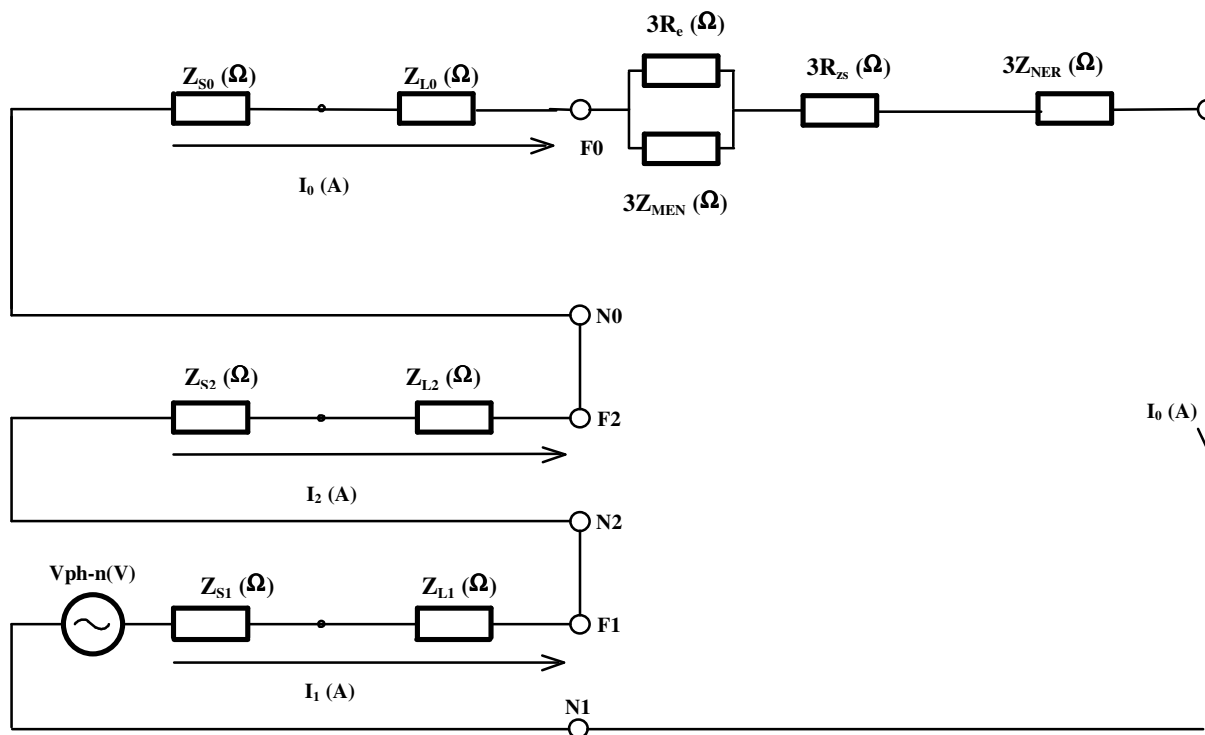


Fig 3.6.1.2 Symmetrical components network for a HV single phase to earth fault at the distribution transformer.

## 11kV SYSTEM DATA

### SOURCE VOLTAGE (volts) & IMPEDANCE (Ohms)

Single phase source voltage  $V_{ph-n}$  (Volts)  $V_{S1} := 6350$   
 Single Phase Fault Level  $S$  (MVA)  $S := 200$   
 Source impedance calculated from the fault level. Assume source impedance is purely reactive and positive sequence = negative sequence = zero sequence.

Positive sequence source impedance (Ohms)  $Z_{S1} := \frac{11^2}{S}j$   $Z_{S1} = 0.6j$   
 Negative sequence source impedance (Ohms)  $Z_{S2} := Z_{S1}$   
 Zero sequence source impedance (Ohms)  $Z_{S0} := Z_{S1}$

### 11kV Overhead line impedance

Conductor size: DOG (6/4.72mm aluminium with 7/1.57mm steel)  
 Length (km)  $L := 1.0$

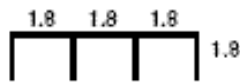
### Line sequence impedances (Ohms/km)

Positive sequence line impedance (Ohms/km)  $Z_{L1} := 0.2722 + 0.3407j$   
 Negative sequence line impedance (Ohms/km)  $Z_{L2} := Z_{L1}$   
 Zero sequence line impedance (Ohms/km)  $Z_{L0} := 0.4204 + 1.6545j$

### 11kV NER AND EARTHING IMPEDANCE (Ohms)

Neutral Earthing Resistor (Ohms)  $Z_{NER} := 0$   
 Zone substation earthing system resistance (Ohms)  $R_{zs} := 0.01$   
 Surface soil resistivity (Ohm-m)  $\rho := 10$  Ohm-m  
 MEN impedance of typical urban extensive MEN system (see HB 219 Worked Example 4.1.1 for the derivation of this value) (Ohms)  $Z_{MEN} := 0.103 + 0.076j$

Distribution transformer earthing system



Transformer earthing system resistance (Ohms)  $R_e := 0.1346 \cdot \rho$   $R_e = 1.3$   
 The equivalent hemispherical radius (m)  $r_E := \frac{\rho}{2 \cdot \pi \cdot R_e}$   $r_E = 1.18$

Equivalent MEN plus  $R_e$  impedance (Ohms)  $Z_{eq} := \left( \frac{1}{Z_{MEN}} + \frac{1}{R_e} \right)^{-1}$

$$Z_{eq} = 0.10 + 0.07j$$

## CALCULATIONS

One Phase to Earth fault on the 11kV feeder at the distribution transformer

Sequence network impedances (Ohms)

$$Z_{\text{pos}} := Z_{S1} + Z_{L1} \cdot L \quad Z_{\text{neg}} := Z_{S2} + Z_{L2} \cdot L \quad Z_{\text{zero}} := Z_{S0} + Z_{L0} \cdot L + 3 \cdot Z_{\text{eq}} + 3 \cdot R_{Zs}$$

$$Z_{\text{pos}} = 0.3 + 0.9j \quad Z_{\text{neg}} = 0.3 + 0.9j \quad Z_{\text{zero}} = 0.7 + 2.5j$$

Zero sequence fault current (Amps)

$$I_0 := \frac{V_{S1}}{Z_{\text{pos}} + Z_{\text{neg}} + Z_{\text{zero}} + 3 \cdot Z_{\text{NER}}}$$

Fault current (Amps).

$$I_f := 3 \cdot I_0$$

$$I_f = 1196.8 - 4026.5j$$

$$|I_f| = 4200.6$$

EPR at the distribution transformer (Volts)

$$EPR_{dt} := I_f \cdot Z_{\text{eq}}$$

$$|EPR_{dt}| = 499$$